

# **Selection and Sensitivity Analysis of Flare Piping Materials for the Onshore Hydrocarbon Industry**

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**Abstract:** In the hydrocarbon industry, Optimal design and development of an onshore plant depends on the correct material selection for piping systems. In the perspective of global warming, every hydrocarbon plant needs an efficient flare system. The efficiency, longevity and cost-effective design comes through proper material selection. To avoid the fatigue failure of the flare system needs a suitable piping design considering mechanical properties. In the managerial aspect, a company focuses on supply lead time and money. In this paper, a certain number of alternative flare pipes are chosen by the optimization process considering important criteria. The technical, economic and supply time is the important pillar of the designing process. Due to the entropy process and sensitivity analysis, the results are more accurate as well as the design process is smooth. The methodology of Simple Additive Weighting (SAW) and Technique for Order Preference by Similarity to Ideal Solution (TOPSIS) are implemented first time and comparative Analysis is to find out the best material for better product development.

**Keywords:** Flare system; Material Selection; Sensitivity Analysis; Entropy; SAW; TOPSIS; Onshore; Hydrocarbon industry

# 1. Introduction

Improperly designed flares may emit methane, sulphur and other volatile organic compounds which creates the problem of our respiratory system and this impact is negatively in environment. This pressure safety device work properly when materials selection goes through scientifically. Economically and proper technically designed flare system is viable for present market scenario. Undesired flammable gases are burnt by flare system, so the essential designing is should be needed through suitable material selection. In practical world, a decision maker has to choose on one among the multiple alternative projects. Specially in piping selection process, it is very difficult task to selection and evaluation of the proposed pipe.

The material selection methodologies are reviewed for replacing the existing material to select a right candidate material of Flare system of hydrocarbon industry, the selection of material methodologies presented in this article contains important selection attributes and its applications

- ✓ Sotoodeh, K. (2022) trying to research of Flare Piping Material Selection for the Offshore Oil and Gas Industry.
- ✓ L. Anoj kumar et. al. (2014) proposed Comparative analysis of MCDM methods for pipe material selection in sugar industry.
- ✓ Ram Narayanaswamy (2017) presented the methodology of the process of materials selection for pipeline systems optimization for life cycles.
- ✓ Jamil Ahmad et. al. (2015) approaches the multi-criteria group decision making for pipe material selection: comparative analysis of hf-vikor and hf-electre ii.

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# 2. Methodology

# 2.1 Multi Criteria Decision Making (MCDM)

Considering multiple conflicting criteria, selecting the best path from a set of feasible alternatives known as Multiple criteria decision making (MCDM). This process always goes through at least two alternatives and two conflicting criteria. MCDM are divided two broad categories: Multiple Attribute Decision Making (MADM) and Multiple Objective Decision Making (MODM). Several useful tools for solving of MCDM problems are

- Simple Additive Weighting method (SAW)
- Technique for Order Preference by Similarity to Ideal Solution (TOPSIS)
- Multi Objective Optimization Ratio Analysis (MOORA)
- Analytical Hierarchy Method (AHP)
- Analytical Network Method ANP etc.

# 2.2 Simple Additive Weighting (SAW)

# Step 1 Formation of decision matrix

Final result of Decision Matrix comprised of a set of columns and rows as well as alternatives and criteria respectively. The decision matrix is a central structure of the MCDA/MCDM since it contains the data for comparison of decision alternatives.

$$\mathbf{C_{1}} \qquad \mathbf{C_{J}} \qquad \mathbf{C_{n}}$$

$$A_{1} \begin{bmatrix} x_{11} & \cdots & x_{1j} & \cdots & x_{1n} \\ \vdots & \cdots & \vdots & \cdots & \vdots \\ x_{i1} & \cdots & x_{ij} & \cdots & x_{in} \\ \vdots & \cdots & \vdots & \cdots & \vdots \\ A_{m} \begin{bmatrix} x_{m1} & \cdots & x_{mj} & \cdots & x_{mn} \end{bmatrix}$$

 $x_{ij}$  is the performance rating of alternative *i* with respect to criterion *j*,

 $A_j \mbox{ is } i^{th} \mbox{ alternative, } C_j \mbox{ is the } j^{th} \mbox{ criterion}$ 

Step 2 Formation of Weight Matrix

Different importance weights to various criteria may be awarded by the decision makers. These importance weights form the weight as follows.

$$W = \begin{bmatrix} W_1 & \cdots & W_j & \cdots & W_n \end{bmatrix}$$

Step 3 Normalization of performance rating

Units and dimensions of performance ratings of columns under criteria differ. For the purpose of comparison, these performance ratings are converted into dimensionless units by normalization using following equations

$$\overline{x}_{ij} = \frac{x_{ij}}{\max_{i}(x_{ij})} \text{ for benefit criteria} j$$

$$\overline{x}_{ij} = \frac{\min_{i}(x_{ij})}{x_{ij}} \text{ for non-benefit criteria} j$$

Normalized decision matrix

$$\overline{X} = \begin{matrix} A_1 \\ \vdots \\ A_2 \\ \vdots \\ A_m \end{matrix} \begin{bmatrix} \bar{x}_{11} \cdots & \dots \cdot \bar{x}_{1j} & \dots & \bar{x}_{1n} \\ \vdots & \vdots & \vdots \\ \bar{x}_{i1} & \dots & \dots \cdot \bar{x}_{ij} & \dots & \bar{x}_{in} \\ \vdots & \vdots & \vdots & \vdots \\ \bar{x}_{m1} & \bar{x}_{mj} & \bar{x}_{mn} \end{matrix} \Bigr|_{m \times n}$$

Step 4 composite score

Computation of composite score  $(CS_i)$  for alternative i

$$CS_i = \sum_{j=1}^n \left( \overline{w}_j * \overline{x}_{ij} \right)$$

Step 5 Ranking and selection of best alternative:

Ranking of products in descending order of composite scores (CS<sub>i</sub>).

# 2.3 Entropy

Entropy was originally a thermodynamic concept, first introduced into information theory by Shannon (see Shannon, 1948 [21]). Widely used in the engineering, socioeconomic and other fields. According to the basic principles of information theory, information is a measure of system's ordered degree, and the entropy is a measure of system's disorder degree. [Table:2]

# 2.4 Sensitivity Analysis

In actual situation decision-making is rather dynamic not static process. Changing with environment it varies in the continuously. In reality the value of decision-making attitude depends upon decision maker's personal choice but now a days the artificial intelligence remove the personal biases. Keeping it in mind, the proposed model for the selection of piping material has been enhanced by sensitivity analysis [Fig:2] to provide a readymade solution of the current problem under variable decision-making attitude. The governing equation of the material measure (AM) is given by

$$AM_i = \alpha (OFM_i - SFM_i) + SFM_i$$

where, i = 1, 2...m.

 $OFM_i$  = Objective factor measure for the alternative i

 $SFM_i$  = Subjective factor measure for the alternative i

 $\alpha$  = Objective factor decision weight/Coefficient of attitude

#### 2.5 Technique for Order Preference by Similarity to Ideal Solution (TOPSIS)

TOPSIS is an evaluation method that is often used to solve number of applications in practice, such as comparison of company performances, financial ratio performance within a specific industry and financial investment in advanced manufacturing systems, etc.

Algorithm of TOPSIS method under MCDM

The idea of TOPSIS can be expressed in a series of steps:

**Step1** All the original criteria receive tendency treatment. We usually transform the cost criteria into benefit criteria, which is shown in detail as follows;

(i) The reciprocal ratio method (X ij = 1/X ij), refers to the absolute criteria;

(ii) The difference method (X ij = 1 - X ij), refers to the relative criteria.

After tendency treatment, construct a matrix

$$X' = [X'_{ij}]_{n \times m}, i = 1, 2..., n; \quad j = 1, 2..., m.$$

**Step2** Calculate the normalized decision matrix A. The normalized value *aij* is calculated as

$$\mathbf{A} = [a_{ij}]_{n \times m}, \ a_{ij} = X'_{ij} / \sqrt{\sum_{i=1}^{n} (X'_{ij})^2} \quad i = 1, 2..., n; \quad j = 1, 2..., m.$$

Step3 Determine the positive ideal and negative ideal solution from the matrix A.

$$\mathbf{A}^{+} = (a_{i1}^{+}, a_{i2}^{+}, \dots, a_{im}^{+}), a_{ij}^{+} = \max_{1 \le i \le n} (a_{ij}), \quad j = 1, 2 \dots, m$$
$$\mathbf{A}^{-} = (a_{i1}^{-}, a_{i2}^{-}, \dots, a_{im}^{-}), a_{ij}^{-} = \min_{1 \le i \le n} (a_{ij}), \quad j = 1, 2 \dots, m$$

**Step4** Calculate the separation measures, using the *n*-dimensional Euclidean distance. The separation of each alternative from the positive ideal solution is given as:

$$D_i^+ = \sqrt{\sum_{j=1}^m W_j (a_{ij}^+ - a_{ij})^2}$$

Similarly, the separation from the negative ideal solution is given as

$$D_i^- = \sqrt{\sum_{j=1}^m W_j (a_{ij}^- - a_{ij})^2}$$

Step5 For each alternative, calculate the ratio Ri as:

$$R_i = \frac{D_i^-}{D_i^- + D_i^+} \quad i = 1, 2 \dots, n$$

Step 6 Rank alternatives in increasing order according to the ratio value of *Ri* in step5.

# 3. Material

The selection of flare piping elements of hydrocarbon industry considering technical, economic and supply aspects. The paper involves identification of different material [Table:1] that are used in the manufacturing of flare pipe and to give a best result. Similar properties of all materials are tabulated in Table one [Table-1]. Six materials with six important properties are considered. The decision maker has to compare all the materials regarding each aspect and has to judge the best one, and this is difficult decision-making problem. So, these MCDM methods is applied to select optimal piping material in this section.

**Table 1:** Flare Piping materials and its properties, price & supply lead time (Days) for Haldia, WB, India location.

| Material                                | Yield<br>Strength<br>(MPa) | UTS<br>(MPa) | % of elongation<br>-<br>Longitudinal<br>(Minimum) | Hardness<br>(Brinnel) | Cost / Kg<br>(INR) | Supply<br>lead<br>time<br>(Days) |
|---|----------------------------|--------------|---|-----------------------|--------------------|----------------------------------|
| LTCS<br>(ASTM A333 Gr. 6) (M1)          | 240                        | 415          | 30  | 187                   | 90                 | 30                               |
| ASTM SA 312<br>TP316 UNS S31600 (M2)    | 205                        | 515          | 40  | 217                   | 400                | 30                               |
| ASTM SA 213<br>TP310MoLNUNS S31254 (M3) | 310                        | 655          | 35  | 220                   | 1100               | 50                               |
| Inconel 625<br>UNS N06625 (M4)          | 517                        | 930          | 42.50   | 240                   | 3300               | 80                               |
| ASTM A 106<br>GR. A (M5)                | 205                        | 330          | 35  | 241                   | 100                | 20                               |
| ASTM A 106<br>GR. B (M6)                | 240                        | 415          | 30  | 241                   | 80                 | 73                               |

# 4. Research Gap

A flare system provided in a refinery or petrochemical plant to ensure the safe and efficient disposal of relieved gases or liquids. Maximum hydrocarbon industry is spent their money to developed an efficient flare system. This paper is projected to improve the flare system through proper material selection.

According to literature review, material selection of Flare system in hydrocarbon industry less work has been done. Although some piecemeal work on this research has been done.

Comparative analysis by various MCDM methods on Material selection process and Sensitivity analysis are implemented first to know the best material as well as the value of closeness.

# 5. Problem Formulation

In industrial environment, flare piping materials are made of carbon steel as well as stainless Steel. Among these six criteria- Yield strength, Ultimate tensile strength, Hardness are beneficiary, and rest of criteria are non- beneficiary.

A hydrocarbon industry has got six different materials with different specifications for flare pipe. The decision maker considered six selection criteria.

# 6. Experiment and Result

In entropy method, the assessment of weightage value is to be determined.

#### Table 2: The weighted values are:

|                 | Yield<br>Strength<br>(MPa) | Ultimate tensile<br>strength (MPa) | % of elongation -<br>(Longitudinal) | Hardness<br>(Brinell) | Cost / Kg<br>(INR) | Supply lead<br>time (Days) |
|-----------------|----------------------------|------------------------------------|-------------------------------------|-----------------------|--------------------|----------------------------|
| weighted values | 0.0823                     | 0.1130                             | 0.0838                              | 0.0503                | 0.5105             | 0.1601                     |

6.1 In the SAW method

The weighted values got from entropy method

STEP1: Determination of normalized decision matrix

| Material                               | Yield<br>Strength<br>(MPa) | Ultimate<br>tensile<br>strength<br>(MPa) | % of elongation -<br>(Longitudinal) | Hardness<br>(Brinell) | Cost / Kg<br>(INR) | Supply lead<br>time (Days) |
|--|----------------------------|--|-------------------------------------|-----------------------|--------------------|----------------------------|
| LTCS<br>(ASTM A333<br>Gr. 6)           | 0.4642                     | 0.4462                                   | 0.7059                              | 1.0000                | 0.8889             | 0.6667                     |
| ASTM SA 312<br>TP316 UNS<br>S31600     | 0.3965                     | 0.5538                                   | 0.9412                              | 0.8618                | 0.2000             | 0.6667                     |
| ASTM SA 213<br>TP310MoLN<br>UNS S31254 | 0.5996                     | 0.7043                                   | 0.8235                              | 0.8500                | 0.0727             | 0.4000                     |
| Inconel 625<br>UNS N06625              | 1.0000                     | 1.0000                                   | 1.0000                              | 0.7792                | 0.0242             | 0.2500                     |
| ASTM A 106<br>GR. A                    | 0.3965                     | 0.3548                                   | 0.8235                              | 0.7759                | 0.8000             | 1.0000                     |
| ASTM A 106<br>GR. B                    | 0.4642                     | 0.4462                                   | 0.7059                              | 0.7759                | 1.0000             | 0.0274                     |

| Material                               | Yield<br>Strength<br>(MPa) | Ultimate<br>tensile<br>strength<br>(MPa) | % of<br>elongation -<br>(Longitudinal) | Hardness<br>(Brinell) | Cost / Kg<br>(INR) | Supply lead<br>time (Days) |
|--|----------------------------|--|--|-----------------------|--------------------|----------------------------|
| LTCS<br>(ASTM A333 Gr. 6)              | 0.0382                     | 0.0504                                   | 0.0592                                 | 0.0503                | 0.4537             | 0.1068                     |
| ASTM SA 312<br>TP316 UNS S31600        | 0.0326                     | 0.0626                                   | 0.0789                                 | 0.0433                | 0.1021             | 0.1068                     |
| ASTM SA 213<br>TP310MoLN<br>UNS S31254 | 0.0494                     | 0.0796                                   | 0.0690                                 | 0.0427                | 0.0371             | 0.0641                     |
| Inconel 625<br>UNS N06625              | 0.0823                     | 0.1130                                   | 0.0838                                 | 0.0392                | 0.0124             | 0.0400                     |
| ASTM A 106<br>GR. A                    | 0.0326                     | 0.0401                                   | 0.0690                                 | 0.0390                | 0.4084             | 0.1601                     |
| ASTM A 106<br>GR. B                    | 0.0382                     | 0.0504                                   | 0.0592                                 | 0.0390                | 0.5105             | 0.0044                     |

STEP 2: Determination of weighted normalized decision matrix

Table 4: weighted normalized decision matrix

STEP 3: Computation of composite score s.... by sum of all weighted normalized rows

The values of (s) are:

| Table 5: | Ccomposite | score |
|----------|------------|-------|
|----------|------------|-------|

| Material | LTCS<br>(ASTM<br>A333<br>Gr. 6) | ASTM SA<br>312<br>TP316 UNS<br>S31600 | ASTM SA 213<br>TP310MoLN<br>UNS S31254 | Inconel 625<br>UNS N06625 | ASTM A 106<br>GR. A | ASTM A 106<br>GR. B |
|----------|---------------------------------|---------------------------------------|--|---------------------------|---------------------|---------------------|
|          | 0.7586                          | 0.4263                                | 0.3419                                 | 0.3707                    | 0.7493              | 0.7017              |





# 6.2 Sensitivity Analysis

Table 6: The value of closeness co-efficient in SAW method

| Material    | when alpha=0 | when alpha=1 |  |
|-------------|--------------|--------------|--|
| LTCS        |              |              |  |
| (ASTM A333  | 0.6108       | 0.1478       |  |
| Gr. 6)      |              |              |  |
| ASTM SA 312 |              |              |  |
| TP316 UNS   | 0.2522       | 0.1741       |  |
| S31600      |              |              |  |
| ASTM SA 213 |              |              |  |
| TP310MoLN   | 0.1439       | 0.1980       |  |
| UNS S31254  |              |              |  |
| Inconel 625 | 0.0916       | 0.2701       |  |
| UNS N06625  | 0.0910       | 0.2771       |  |
| ASTM A 106  | 0.6075       | 0.1418       |  |
| GR. A       | 0.0075       | 0.1418       |  |
| ASTM A 106  | 0 5539       | 0.1/78       |  |
| GR. B       | 0.5557       | 0.1470       |  |



Figure 2. Sensitivity Analysis in SAW

# 6.3 In the TOPSIS method

| Material                               | Yield<br>Strength<br>(MPa) | Ultimate<br>tensile strength<br>(MPa) | % of elongation -<br>(Longitudinal) | Hardness<br>(Brinell) | Cost / Kg<br>(INR) | Supply lead<br>time (Days) |
|--|----------------------------|---------------------------------------|-------------------------------------|-----------------------|--------------------|----------------------------|
| LTCS<br>(ASTM A333<br>Gr. 6)           | 0.4642                     | 0.4462                                | 0.7059                              | 1.0000                | 0.8889             | 0.6667                     |
| ASTM SA 312<br>TP316 UNS<br>S31600     | 0.3965                     | 0.5538                                | 0.9412                              | 0.8618                | 0.2000             | 0.6667                     |
| ASTM SA 213<br>TP310MoLN<br>UNS S31254 | 0.5996                     | 0.7043                                | 0.8235                              | 0.8500                | 0.0727             | 0.4000                     |
| Inconel 625<br>UNS N06625              | 1.0000                     | 1.0000                                | 1.0000                              | 0.7792                | 0.0242             | 0.2500                     |
| ASTM A 106<br>GR. A                    | 0.3965                     | 0.3548                                | 0.8235                              | 0.7759                | 0.8000             | 1.0000                     |
| ASTM A 106<br>GR. B                    | 0.4642                     | 0.4462                                | 0.7059                              | 0.7759                | 1.0000             | 0.0274                     |

# **STEP1:** Determination of normalized decision matrix **Table 7:** Normalized decision matrix

**STEP 2:** Determination of positive ideal solution: taking the maximum values of each column from the normalized decision matrix

# Table 8: positive ideal solution

| Yield<br>Strength<br>(MPa) | Ultimate tensile<br>strength (MPa) | % of elongation -<br>(Longitudinal) | Hardness<br>(Brinell) | Cost / Kg<br>(INR) | Supply lead<br>time (Days) |
|----------------------------|------------------------------------|-------------------------------------|-----------------------|--------------------|----------------------------|
| 1                          | 1                                  | 1                                   | 1                     | 1                  | 1                          |

Determination of negative ideal solution: taking the minimum values of each column from the normalized decision matrix

# Table 9: Negative ideal solution

| Yield<br>Strength<br>(MPa) | Ultimate tensile<br>strength (MPa) | % of elongation -<br>(Longitudinal) | Hardness<br>(Brinell) | Cost / Kg<br>(INR) | Supply lead<br>time (Days) |
|----------------------------|------------------------------------|-------------------------------------|-----------------------|--------------------|----------------------------|
| 0.3965                     | 0.3548                             | 0.7059                              | 0.7759                | 0.0242             | 0.0274                     |

| Material | LTCS<br>(ASTM<br>A333<br>Gr. 6) | ASTM SA<br>312<br>TP316 UNS<br>S31600 | ASTM SA 213<br>TP310MoLN<br>UNS S31254 | Inconel 625<br>UNS N06625 | ASTM A 106<br>GR. A | ASTM A 106<br>GR. B |
|----------|---------------------------------|---------------------------------------|--|---------------------------|---------------------|---------------------|
|          | 0.2994                          | 0.6310                                | 0.7234                                 | 0.7606                    | 0.3203              | 0.4685              |

Table 10: Calculation of the separation measure from the positive ideal solution(di\_Plus)

| Table 11 | . Calculation | of the separation | measure from th | e negative ideal | solution(di_ | Minus) |
|----------|---------------|-------------------|-----------------|------------------|--------------|--------|
|----------|---------------|-------------------|-----------------|------------------|--------------|--------|

| Material | LTCS<br>(ASTM<br>A333<br>Gr. 6) | ASTM SA<br>312<br>TP316 UNS<br>S31600 | ASTM SA 213<br>TP310MoLN<br>UNS S31254 | Inconel 625<br>UNS N06625 | ASTM A 106<br>GR. A | ASTM A 106<br>GR. B |
|----------|---------------------------------|---------------------------------------|--|---------------------------|---------------------|---------------------|
|          | 0.6715                          | 0.3011                                | 0.2051                                 | 0.3036                    | 0.6781              | 0.6981              |

STEP 3: Calculation of R\_i

Table 12: Calculation of R\_i

| Material | LTCS<br>(ASTM<br>A333<br>Gr. 6) | ASTM SA<br>312<br>TP316 UNS<br>S31600 | ASTM SA 213<br>TP310MoLN<br>UNS S31254 | Inconel 625<br>UNS N06625 | ASTM A 106<br>GR. A | ASTM A 106<br>GR. B |
|----------|---------------------------------|---------------------------------------|--|---------------------------|---------------------|---------------------|
|          | 0.6916                          | 0.3231                                | 0.2209                                 | 0.2853                    | 0.6792              | 0.5984              |

STEP 4: Arranging the final value in descending order:----->>> M1 > M5 > M6 > M2 > M4 > M3



Figure 3. Material ranking in TOPSIS

|                           | SAW    | TOPSIS |  |
|---------------------------|--------|--------|--|
| MATERIAL                  | (RANK) | (RANK) |  |
| LTCS                      |        | 1      |  |
| (ASTM A333 Gr. 6) (M1)    | 1      |        |  |
| ASTM SA 312               | 4      | 4      |  |
| TP316 UNS S31600 (M2)     | 4      | 4      |  |
| ASTM SA 213               | 6      | 6      |  |
| TP310MoLN UNS S31254 (M3) | 0      |        |  |
| Inconel 625               | 5      | 5      |  |
| UNS N06625 (M4)           | 5      | 5      |  |
| ASTM A 106                | 2      | 2      |  |
| GR. An (M5)               | 2      |        |  |
| ASTM A 106                | 3      | 3      |  |
| GR. B (M6)                | 5      |        |  |

Table 13. Comparative analysis of ranking of Piping materials using MCDM methods

# 7 Discussion

From the result we see that for the two different processes of MCDM, the result is same. The ranking of 1<sup>st</sup> to 6<sup>th</sup> materials are same for those two different processes. In SAW and TOPSIS methods, ranks of alternatives are given in descending order of their respective composite score. So, the ranking of alternatives of materials are as follows: M1 > M5 > M6 > M2 > M4 > M3. It means that Material 1 is the best as it maximizes the benefit criteria.

We have also made the sensitivity analysis with graphical representation in which we see that in SAW method. From the sensitivity analysis graph, we also get the rank of the lathes for any alpha value by drawing a vertical line from that alpha value to the straight line of the lathe in the graph. That's why for doing the sensitivity analysis our result does not depends any different decision makers with their different weighted values.

# 8 Conclusions

A flare system is defined as per CAPP (Canadian Association of Petroleum Producers), the controlled burning of natural gas that cannot be processed for sale or use because of technical or economic reasons. It is quite clear that selection of a proper flare piping material for a given manufacturing application goes through a large number of considerations. The use of SAW and TOPSIS methods are observed to be quite capable and computationally easy to evaluate and select the proper material from a given set of alternatives. These methods use the measures of the considered criteria with their relative importance in order to arrive at the final ranking of the alternative material. Thus, these popular MCDM methods can be successfully employed for solving any type of decision-making problems having any number of criteria and alternatives in the manufacturing domain. As a future scope, a fuzzy TOPSIS, fuzzy SAW based methodology may be developed to aid the decision makers to take decisions in presence of imprecise and incomplete data.

# **Declaration By Authors**

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